# The Modulus of a Cross Linked Melt

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## History

The problem of permanent cross links (see figure 1), where  $\mathbf{r}(s_b^a) = \mathbf{r}(s_a^b)$ , and that of entanglements, where  $I_{ab}([\mathbf{r}_a][\mathbf{r}_b]) = I_{ab}([\mathbf{r}_a^{-1}][\mathbf{r}_b^{-1}])$ , is how to determine the modulus, G:

$$G = G' + iG''$$

$$G = G(\omega, c_x, c_e)$$
 (1)

where  $c_x = \frac{N_x}{V}$  and  $c_e = \frac{\sum I}{V}$ .

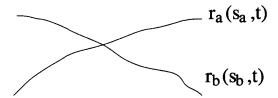


Figure 1:

The problem is that we need to obtain  $F_{expt}$ , where

$$F_{expt} = \langle F([s_b^a], I_{ab}) \rangle \tag{2}$$

$$= \left\langle kT \log \int \exp\left(-H/kT\right) \prod \left[ \frac{\delta \left(r_{\rm a}^{\rm b} - r_{\rm b}^{\rm a}\right)}{\delta \left(I - J\right)} \right] \right\rangle \tag{3}$$

i.e.

$$F_{expt} = \langle \log Z \rangle \tag{4}$$

$$\neq \log \langle Z \rangle$$
 (5)

If  $F(n) = \langle Z^n \rangle$ , then

$$\left. \frac{\partial F}{\partial n} \right|_{n=0} = \langle F \rangle \tag{6}$$

This is the extension of the Gibbs method (equivalent to the replica method). It cannot give G. We therefore need a dynamical solution. The dynamical problem needs extensions of the Boltzmann (Smoluchowski, Langevin, Fokker-Planck) equation.

### Method

The method is to use the Rayleighan (or Rayleighs friction function).

$$\mathcal{R}_0 = L + M + \sum \lambda C \tag{7}$$

where L is the Lagrangian, M is the friction function,  $\lambda$  are the Lagrange multipliers, and C are the associated constraints. Rayleigh showed that:

$$\frac{\delta L}{\delta r} + \frac{\delta M}{\delta u} + \sum \lambda \frac{\delta C}{\delta r} = 0 \tag{8}$$

where  $u = \dot{r}$ , but is only identified at the end.

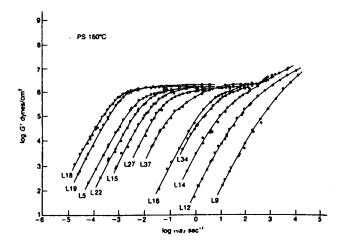


Figure 2: Experimental data from Onogi, Masuda and Kitagawa, *Macromolecules*, 3, 109 (1970)

### **Problem**

The problem is to predict the experimental curve

$$G'(c_e) > G'(c_e = 0) \tag{9}$$

A simple qualitative explanation can be seen in figure 4.

## Model

 $n=n\left(s\right)$ . The axis of the tube, the primitive path, is described by  $\mathbf{R}(\mathbf{n}\left(\mathbf{s}\right),\mathbf{t})$ . The Rayleighan involves  $\mathbf{r},\dot{\mathbf{r}},\mathbf{R},\dot{\mathbf{R}}$ .

The potential function is given by:

$$U = \frac{3kT}{2L} \int_0^L \left[ \left( \frac{\partial \mathbf{r}}{\partial s} \right)^2 + q_1^2 \left( \mathbf{r} - \mathbf{R} \right)^2 \right]$$
 (10)

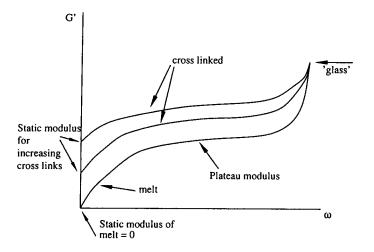


Figure 3:

and the constraint

$$\int_{0}^{L} \frac{\partial n}{\partial s} ds = N \tag{11}$$

where aN is the length of the tube.

The relative velocities are given by:

$$\left(\frac{d\mathbf{r}}{dt} - \frac{d\mathbf{R}}{dt}\right)\Big|_{\mathbf{fixed s}} = \left(\dot{\mathbf{r}} - \frac{\partial \mathbf{R}}{\partial n}\dot{n} - \dot{\mathbf{R}}\right) \tag{12}$$

this velocity  $\times \zeta$  gives the friction of a chain segment within its environment.

$$\left. \left( \frac{d\mathbf{R}}{dt} \bigg|_{s} - \frac{\partial \mathbf{R}}{\partial t} \bigg|_{n} \right) \to \frac{\partial \mathbf{R}}{\partial n} \dot{n}$$
 (13)

Equation 13 is the slip motion along the primitive path, and has friction  $\nu$ .

Therefore, the Rayleighan becomes:

$$\mathcal{R}_{0} = -U - \frac{1}{2} \zeta \int ds \left( \dot{\mathbf{r}} - \mathbf{R}' \dot{\mathbf{n}} - \dot{\mathbf{R}} \right)^{2} - \frac{1}{2} \nu \int ds \left( \mathbf{R}' \dot{\mathbf{r}} \right)^{2}$$
(14)

and from Rayleighs equations, we obtain:

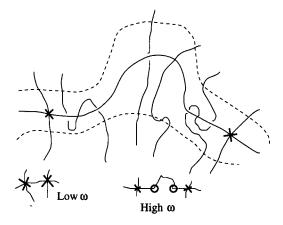


Figure 4:

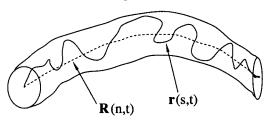


Figure 5:

$$\zeta \left( \dot{\mathbf{r}} - \frac{\partial \mathbf{R}}{\partial n} \dot{n} - \dot{\mathbf{R}} \right) + \frac{3kT}{L} \left( -\frac{\partial^2 \mathbf{r}}{\partial s^2} + q_1^2 (\mathbf{r} - \mathbf{R}) \right) = \mathbf{0}$$

$$\left( \partial \mathbf{R} \right)^2 \dots 3kT \partial \mathbf{R} \left( -\frac{\partial^2 \mathbf{r}}{\partial s^2} \right) = \mathbf{0}$$
(15)

$$\nu \left(\frac{\partial \mathbf{R}}{\partial n}\right)^{2} \dot{n} + \frac{3kT}{L} \frac{\partial \mathbf{R}}{\partial n} \left(-\frac{\partial^{2} \mathbf{r}}{\partial s^{2}}\right) = 0$$
 (16)

Now put  $\tilde{\mathbf{r}}(st) = \mathbf{r}(st) - \mathbf{R}(n, t)$ , and ignore  $\tilde{\mathbf{r}}$ , to obtain:

$$\nu \left(\frac{\partial \mathbf{R}}{\partial n}\right)^2 \dot{n} + \frac{3kT}{L} \left(\frac{\partial \mathbf{R}}{\partial n}\right) \cdot \left(-\frac{\partial^2 \mathbf{R}}{\partial s^2}\right) = 0 \tag{17}$$

The static equilibrium solution is:

$$R_0 \sim an(s,t), \quad \frac{\partial^2 n}{\partial s^2} = 0$$
 (18)

and

$$n_0 = \frac{N}{L}s\tag{19}$$

for uniform progression.

## **Deformation**

The deformation is given by a linear theory:

$$\mathbf{R} = \underline{E}(t)\,\mathbf{R}_0 \cong \mathbf{R}_0 + \underline{\varepsilon} \cdot \mathbf{R}_0 \tag{20}$$

$$n\left(st\right) = n_0 + n_1 \tag{21}$$

$$\frac{l\nu}{3kT} \left( \frac{\partial n_1}{\partial t} \right) - \frac{\partial^2 n_1}{\partial s^2} = \left( \frac{N}{aL} \right)^2 \frac{\partial \mathbf{R}_0}{\partial n} \left( \varepsilon + \varepsilon^T \right) \frac{\partial \mathbf{R}_0}{\partial n}$$
 (22)

where the right hand side of the last equation represents the source of  $n_1$  changes.

### Stress

We have the usual formula:

$$\sigma_{ij} = c_x \left( \frac{3kT}{l} \right) \int_0^L ds \left\langle \frac{\partial r_i}{\partial s} \frac{\partial r_j}{\partial s} \right\rangle \tag{23}$$

where

$$\mathbf{r}\left(s,t\right) \cong \mathbf{R}_{0}\left(n_{0}\right) + \underline{\underline{\varepsilon}}\mathbf{R}_{0} + \left(\frac{\partial \mathbf{R}_{0}}{\partial n_{0}}\right) n_{1}\left(s,t\right) \tag{24}$$

and

$$\mathbf{r} \cong \mathbf{R}_0 + \underline{\underline{\varepsilon}} \cdot \mathbf{R}_0 + \left(\frac{\partial \mathbf{R}_0}{\partial \mathbf{n}_0}\right) \mathbf{n}_1 \tag{25}$$

where the first term of equation (25) gives zero effect from thermodynamic theory and the second term corresponds to the stress,  $G(\omega \to 0)$ . For a random walk on a primitive path, we have

$$\left\langle \frac{\partial R_{0i}}{\partial s} \frac{\partial R_{0j}}{\partial s} \right\rangle = \left( \frac{N}{L} \right)^2 \frac{a^2}{3} \delta_{ij} \tag{26}$$

and using the fact that  $Na^2 = Ll$ , we have

$$\underline{\sigma} = (c_x N) k T \underline{\varepsilon} (t) \tag{27}$$

The third term of equation 25 corresponds to the relaxation.

$$n_1 = \int_a^L G\left(ss'\right) \tag{28}$$

with a source term

$$\left(\frac{N}{aL}\right)^2 \frac{\partial R_0}{\partial n} \left(\varepsilon + \varepsilon^T\right) \frac{\partial R_0}{\partial n} \tag{29}$$

 $\mathbf{and}$ 

$$\left(\frac{l\nu}{3kT}i\omega - \frac{\partial^2}{\partial s^2}\right)G = \delta\left(s - s'\right). \tag{30}$$

## Final Result

Take the case of  $\epsilon_{\alpha\beta}=\epsilon_{\alpha\beta}^{0}Re\left(\exp\left(i\omega t\right)\right)$ 

$$\sigma = c_x NkT \underline{\underline{\varepsilon}}^0 Re \left[ 2 - \frac{2}{5} \frac{1}{x} f(x, N) \exp(i\omega t) \right]$$
 (31)

where

$$x = \exp(i\pi/4)\sqrt{\frac{l\nu\omega}{kT}}\left(\frac{L}{N}\right)$$
 (32)

and

$$f\left(x,N\right)=1-\exp\left(-x\right)-\frac{2\exp\left(-nX\right)}{\sinh\left(Nx\right)}\sinh^{2}\left(\frac{x}{2}\right)-\frac{1}{N}\tanh\left(\frac{x}{2}\right) \tag{33}$$

The diffusion of the primitive path is characterised by the time:

$$\tau = \frac{1}{2} \frac{l\nu}{3kT} \left(\frac{L}{N}\right)^2 \tag{34}$$

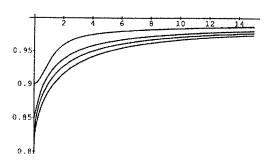


Figure 1:  $G'/[2k_BT(c_x+c_e)]$  versus  $\tau_{L/N}\omega$ . From top to bottom,  $N=1+c_e/c_r=1,2,4,8,\infty$ .

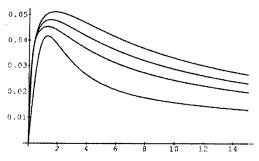


Figure 2:  $G''/[2k_BT(c_x+c_c)]$  versus  $\tau_{L/N}\omega$ . From bottom to top,  $N=1+c_c/c_r=1,2,4,3,\infty$ .

Figure 6:

Consider the following specific example. Let  $\varepsilon_{xx}=\varepsilon_{yy}=0,$  and  $\varepsilon_{zz}=\varepsilon^0Re\left(\exp\left(i\omega t\right)\right).$ 

Also, let  $\sigma_{zz}=Re\left(G^{*}\varepsilon^{0}\exp\left(i\omega t\right)\right)$ , where

$$G^* = (c_x N) kT \left(2 - \frac{2}{5} \frac{1}{x} f(x, N)\right)$$

$$\tag{35}$$

In equation (35),

 $c_x \equiv \text{number of chains per unit volume}$ 

 $c_x N \equiv \text{number of steps of primitive path per unit volume}$ 

(36)

i.e.,  $c_x$  is the density of cross links, and  $c_xN$  is the density of crosslinks plus the density of the entanglements, so  $c_xN=c_x+c_e$ .

There are a number of limiting cases:

1. 
$$\frac{c_x}{c_x} = 0$$
  $G^* = 2c_x kT$  (i.e.  $N = 1$ ) (37)

2. 
$$\frac{c_x}{c_x} \to \infty$$
  $G^* = 2 (c_x + c_e) kT \left[ 1 - \frac{1}{5} \frac{(1 - \exp(-x))}{x} \right]$  (i.e.  $N = \infty$ ) (38)

3. 
$$G^*(\omega \to \infty) = 2uT(c_x + c_e)$$
 (plateau) (39)

4. 
$$G^*(\omega \to 0) = 2kT\left(c_x + \frac{4}{5}c_e\right)$$
 (for large  $Nc_e >> c_x$ , therefore  $\frac{8}{5}\left(c_xN\right)kT$ ) (40)

For the general Rayleighan problem, consider the simple case of unentangled chains:  $\mathbf{r}(s_b^a) = \mathbf{r}(s_b^b)$ 

$$\mathcal{R} = -\sum_{a} \frac{3kT}{2l} \int \left(\frac{\partial r_{a}}{\partial s_{a}}\right)^{2} \frac{ds}{dt} + \sum_{a,b} \int \lambda_{ab} \left(t\right) \left(r_{a} \left(s_{a}^{b} t\right) - r_{b} \left(s_{b}^{a} t\right)\right) dt + \sum_{a} \frac{m}{2} \int \dot{r}_{a}^{2} \left(s_{a}\right) ds_{a} dt + \frac{\nu}{2} \int \tilde{v}_{a}^{2} ds_{a} dt + \text{Noise source}$$
(41)

where  $\tilde{v} = v - \bar{v}$  is the average velocity.

This gives:

$$\rho \ddot{r}_a + \nu \frac{\partial}{\partial t} (r_a - \bar{r}_a) + \frac{3kT}{l} \frac{\partial^2 r_a}{\partial s_a^2} + \sum_b \lambda_{ab} \delta \left( s_a - s_a^b \right) = f_a$$
 (42)

and we model the sum by  $rac{3kT}{l}q_0^2\left(r_i-ar{r}_i
ight)$  to give

$$q_0^2 = \left\langle \sum_b \frac{\delta \left( s_a - s_a^b \right)}{G(0, \omega)} \right\rangle \tag{43}$$

where G is the mean Green function

$$\left[m\omega^2 + i\nu\omega + \frac{3kT}{l}\left(q^2 + q_0^2\right)\right]G = 1 \tag{44}$$

and this yields

$$q_0 = \frac{c_x}{L} \tag{45}$$

The equations above extend the locus of chains into  $\omega$  variation due to the fluctuation of cross link positions.

One can now generalise the earlier model, but the algebra is difficult.